

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE 2982

SUPersonic FLOW PAST OSCILLATING AIRFOILS INCLUDING NONLINEAR THICKNESS EFFECTS

By Milton D. Van Dyke

Ames Aeronautical Laboratory
Moffett Field, Calif.

DISTRIBUTION STATEMENT A
Approved for Public Release
Distribution Unlimited



Washington
July 1953

Reproduced From
Best Available Copy

20000807 185

DMC QUALITY INSPECTED 4

AQM00-08-2465

K
NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE 2982

SUPersonic FLOW PAST OSCILLATING AIRFOILS
INCLUDING NONLINEAR THICKNESS EFFECTS

By Milton D. Van Dyke

SUMMARY

A solution to second order in thickness is derived for harmonically oscillating two-dimensional airfoils in supersonic flow. For slow oscillations of an arbitrary profile, the result is found as a series including the third power of frequency. For arbitrary frequencies, the method of solution for any specific profile is indicated, and the explicit solution derived for a single wedge.

Nonlinear thickness effects are found generally to reduce the torsional damping, and so enlarge the range of Mach numbers within which torsional instability is possible. This destabilizing effect varies only slightly with frequency in the range involved in dynamic stability analysis, but may reverse to a stabilizing effect at high flutter frequencies. Comparison with a previous solution exact in thickness suggests that nonlinear effects of higher than second order are practically negligible.

The analysis utilizes a smoothing technique which replaces the actual problem by one involving no kinked streamlines. This strategem eliminates all consideration of shock waves from the analysis, yet yields the correct solution for problems which actually contain shock waves.

INTRODUCTION

As linearized supersonic-flow theory is increasingly applied to problems of unsteady motion of lifting wings, the results are sometimes advanced with the warning that they may be significantly affected by nonlinear effects of thickness. Such caution is justified because it is known that even for steady flow, linearized theory is often inadequate for predicting the pitching moment - and prediction of moments is one of the main objectives of unsteady-flow theory. It may be anticipated that nonlinear effects will become increasingly important as the Mach number falls toward unity, particularly for slow oscillations.

In the present work the effects of thickness are determined for a harmonically oscillating two-dimensional airfoil by calculating the second-order solution. This is the counterpart for unsteady motion of the well-known steady-flow result of Busemann (ref. 1). First, for slow oscillations a solution is found for an airfoil of arbitrary profile. The result is given as a series which includes terms up to the third power of the frequency. Second, for arbitrarily high frequencies it is shown that a solution can be found for any specific airfoil, and the solution is carried out explicitly for a single wedge. Finally, comparison is made with a previous solution for the wedge which is exact with respect to thickness (refs. 2 and 3), in order to assess the effects of nonlinear terms of higher than second order.

Extensive use is made of a smoothing technique, which replaces the actual problem by one having no kinked streamlines. This strategem, which has been used previously and may prove useful in future problems, eliminates all consideration of shock waves from the analysis. It, nevertheless, leads to the correct second-order solution for the actual problem, which does involve shock waves.

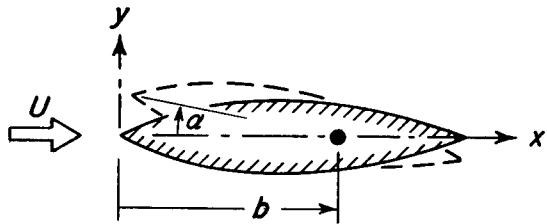
METHOD OF ANALYSIS

Statement of Problem

Consider a uniform supersonic stream flowing past a sharp-nosed airfoil which executes prescribed harmonic oscillations. We shall be concerned with calculating the instantaneous pressure at the surface of the airfoil and, hence, the unsteady lift and pitching moment. It is usually the custom to consider the oscillation to be compounded of a rotation (say about the midchord) and a vertical translation (plunging), which are not generally in phase. However, we shall here limit attention to the special case of the airfoil pivoted about an arbitrary point downstream of its leading edge. This is no real restriction because the plunging case can be recovered by letting the distance to the pivot tend to infinity and the angular amplitude of oscillation tend to zero, their product remaining finite.

Although the iteration procedure to be employed yields a formal result for any Mach number greater than unity, the solution probably breaks down when the flow becomes sonic at any point. Since this occurs at a Mach number somewhat higher than that for bow wave detachment, the upper and lower surfaces of the airfoil operate independently in the probable range of validity of the solution. It is therefore sufficient to consider only the half field of flow lying above the airfoil, and this viewpoint will be adopted henceforth.

Choose the origin of coordinates at the mean position of the leading edge, with the x axis extending in the direction of the free stream (sketch (a)). Then it is convenient to describe the upper surface of the airfoil in its mean (zero angle of attack) position by



Sketch (a).- Coordinate system for oscillating airfoil.

$$y = Y(x) = \epsilon g(x) \quad (1)$$

Here ϵ is a small parameter representative of the airfoil thickness, so that the function g is of order unity. Now let the airfoil pivot about a point lying a distance b downstream from the leading edge, and perform harmonic oscillations of frequency ω and amplitude α_0 , so that the angle of attack, which is the angle between the instantaneous position of the airfoil and its original mean position (sketch (a)), is given by

$$\alpha = \alpha_0 \cos \omega t = \alpha_0 e^{i\omega t} \quad (2)$$

(Here, as in all that follows, it is implied that actual physical quantities are given by the real parts of their complex representations.) Then, at any instant the moving upper surface of the airfoil is described implicitly, to second order in thickness and angle of attack, by

$$y = \epsilon g(x-\alpha y) - (x-b)\alpha \quad (3a)$$

Now, if the airfoil is smooth (so that the function g is differentiable), the equation of the surface can be written explicitly as

$$y = \epsilon g(x) - \alpha_0 e^{i\omega t} (x-b) \quad (3b)$$

with an error of order $(\epsilon^2 \alpha, \epsilon \alpha^2)$, which is of third order and, consequently, negligible in the present second-order analysis.

Perturbation Equation

The entropy changes due to shock waves are of third order in the airfoil thickness and angle of attack. Hence, to second order the flow is irrotational and isentropic. Because it is irrotational, there exists a potential function Ω whose gradient yields the velocity vector:

$$\vec{q} = \text{grad } \Omega, \quad \begin{cases} u = \Omega_x \\ v = \Omega_y \end{cases} \quad (4)$$

Bernoulli's equation for plane unsteady flow can be written (from eqs. (14.04) and (9.06) of ref. 4)

$$\Omega_t + \frac{1}{2} (u^2 + v^2) + \frac{a^2}{\gamma-1} = \frac{a_0^2}{\gamma-1} + \frac{1}{2} U^2 \quad (5)$$

Here a is the speed of sound, and a_0 its value in the free stream, where the flow velocity is U . Differentiating this expression with respect to time t , and using the fact that $d[a^2/(\gamma-1)]/dt = a^2 dp/\rho$ (ref. 4, eqs. (9.03) and (9.06) gives

$$\Omega_{tt} + uu_t + vv_t + \frac{a^2}{\rho} \rho_t = 0 \quad (6)$$

This, together with the corresponding results obtained by differentiating with respect to x and y , can be used to eliminate derivatives of the density from the continuity equation (ref. 4, eq. (7.08.2))

$$\rho_t + (\rho u)_x + (\rho v)_y = 0 \quad (7)$$

The result is that the velocity potential satisfies the equation

$$(a^2 - \Omega_x^2)\Omega_{xx} + (a^2 - \Omega_y^2)\Omega_{yy} - 2\Omega_x\Omega_y\Omega_{xy} - 2\Omega_x\Omega_{xt} - 2\Omega_y\Omega_{yt} - \Omega_{tt} = 0 \quad (8a)$$

where, from equations (4) and (5),

$$a^2 = a_0^2 + \frac{\gamma-1}{2} (U^2 - \Omega_x^2 - \Omega_y^2 - 2\Omega_t) \quad (8b)$$

Now introduce a perturbation potential Φ , normalized through division by the free-stream velocity U , by setting

$$\Omega(x, y, t) = U [x + \Phi(x, y, t)] \quad (9a)$$

so that the velocity components are given by

$$\left. \begin{aligned} \frac{u}{U} &= 1 + \Phi_x \\ \frac{v}{U} &= \Phi_y \end{aligned} \right\} \quad (9b)$$

Then substituting into equations (8) gives

$$(1-M^2)\Phi_{xx} + \Phi_{yy} - 2\frac{M^2}{U}\Phi_{xt} - \frac{M^2}{U^2}\Phi_{tt} = M^2 \left[(\gamma-1) \left(\Phi_x + \frac{\Phi_t}{U} + \frac{\Phi_x^2 + \Phi_y^2}{2} \right) (\Phi_{xx} + \Phi_{yy}) + (2\Phi_x + \Phi_x^2)\Phi_{xx} + \Phi_y^2\Phi_{yy} + 2(1+\Phi_x)\Phi_y\Phi_{xy} + \frac{2}{U}(\Phi_x\Phi_{xt} + \Phi_y\Phi_{yt}) \right] \quad (10)$$

For purposes of a second-order solution (and to higher order a potential does not exist), the triple products on the right-hand side can be disregarded. Thus, the perturbation equation becomes finally

$$\Phi_{yy} - \beta^2\Phi_{xx} - 2\frac{M^2}{U}\Phi_{xt} - \frac{M^2}{U^2}\Phi_{tt} = M^2 \left[(\gamma-1)(\Phi_x + \frac{\Phi_t}{U})(\Phi_{xx} + \Phi_{yy}) + 2\Phi_x\Phi_{xx} + 2\Phi_y\Phi_{xy} + \frac{2}{U}(\Phi_x\Phi_{xt} + \Phi_y\Phi_{yt}) \right] \quad (11)$$

where $\beta^2 = M^2 - 1$.

Pressure Relation

Dividing the Bernoulli equation (eq. (5)) by $a^2/(\gamma-1)$ gives

$$\frac{a^2}{a_0^2} = 1 + \frac{\gamma-1}{2} M^2 \left(1 - \frac{u^2 + v^2 + 2\Omega t}{U^2} \right) \quad (12)$$

The flow is isentropic to second order, so that

$$\frac{p}{p_0} = \left(\frac{a^2}{a_0^2} \right)^{\frac{\gamma}{\gamma-1}}, \quad \frac{p_0}{\frac{1}{2} \rho_0 U^2} = \frac{2}{\gamma M^2}$$

and it follows that the pressure coefficient at any point is given by

$$C_p \equiv \frac{p-p_0}{\frac{1}{2} \rho_0 U^2} = \frac{2}{\gamma M^2} \left\{ \left[1 + \frac{\gamma-1}{2} M^2 \left(1 - \frac{u^2 + v^2 + 2\Omega t}{U^2} \right) \right]^{\frac{\gamma}{\gamma-1}} - 1 \right\} \quad (13)$$

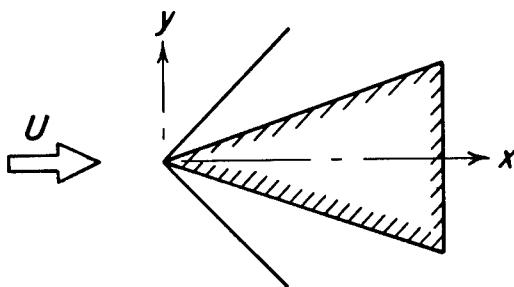
Substituting the velocity components of equation (9b), expanding in series, and retaining only squares and products of perturbation quantities gives finally

$$C_p = -2\Phi_x - 2 \frac{\Phi_t}{U} + \beta^2 \Phi_x^2 - \Phi_y^2 + 2M^2 \Phi_x \frac{\Phi_t}{U} + M^2 \left(\frac{\Phi_t}{U} \right)^2 \quad (14)$$

Here the second-order solution is required only for evaluating the first two terms; the others are given correct to second order by linear theory.

Smoothing of Problem

From the leading edge and from any subsequent corner of the airfoil spring shock waves or Prandtl-Meyer expansion fans which oscillate as the airfoil oscillates. These introduce serious complications into the second-order analysis. However, the complications can all be circumvented by solving a "smoothed" problem in place of the actual problem. The solution can thereupon be applied to the actual problem, for which it yields the correct result everywhere except near the shock waves and Prandtl-Meyer fans.



Sketch (b).- Steady flow past a wedge.

The nature of the difficulties can be understood by considering first the special problem of steady flow past a single wedge (sketch (b)). The presence of the bow shock wave means that the analysis must be undesirably complicated by including the Rankine-Hugoniot relations (in a simplified form). A second complication arises in the differential equation which, for steady flow, becomes

$$\Phi_{yy} - \beta^2 \Phi_{xx} = M^2 \left[(\gamma+1) \Phi_x \Phi_{xx} + (\gamma-1) \Phi_x \Phi_{yy} + 2\Phi_y \Phi_{xy} \right] \quad (15)$$

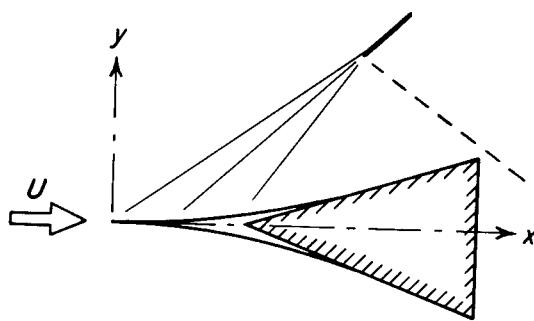
In the iteration procedure to be employed, the nonlinear right-hand side is evaluated in terms of the first-order solution, and the resulting nonhomogeneous wave equation solved for the second-order potential. However, for the wedge the right-hand side vanishes (to any order), which would imply incorrectly that the second-order solution does not involve the adiabatic exponent γ . More precisely, the right-hand side vanishes everywhere except along the Mach lines springing from the apex, where it has the singular behavior of the Dirac delta function, and only by

taking account of these troublesome singularities could the correct solution be found.

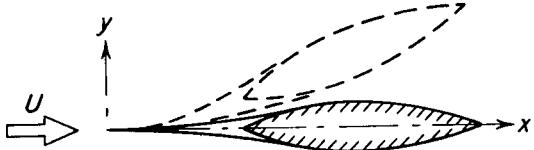
Both these complications are avoided by the simple device of solving the problem of flow past a smooth cusp-nosed airfoil of arbitrary shape and then applying the final solution to the wedge. It may be imagined that the wedge has been smoothed by adding a cusped extension to its nose, as indicated in sketch (c). It is clear that this artifice removes the troublesome singularities from the right-hand side of the differential equation. Likewise, it eliminates the need for the shock-wave relations because, as indicated in sketch (c), with sufficient smoothing, shock waves will form only at such great distance that their effects cannot reach the airfoil surface. Although shock waves are thus apparently excluded, the correct second-order

result for the wedge is nevertheless recovered from the solution by imagining the extension to shrink in size and disappear. The reason is that to second order a shock wave is equivalent to the limit of a rapid continuous isentropic compression. This limiting procedure, which is equivalent simply to applying the solution for an arbitrary smooth shape to one which is not smooth, yields the proper result except in the vicinity of the shock wave (see ref. 5). For an airfoil of general shape, similar broad smoothing must be imagined at any concave corner; whereas at convex corners (since no shock waves form) the slightest rounding is enough. This smoothing technique was applied in reference 4 (p. 399) to steady first-order flow past bodies of revolution, and in reference 5 to steady second-order plane flow.

We turn now to the question of generalizing this smoothing scheme to an oscillating airfoil. Modification is necessary only at the leading edge. Consider first the special case of rotation about the leading edge. Then it is enough to conceive of an extension which is flexible, so that its cusped tip can be maintained fixed and directed always into the free stream while the airfoil oscillates, as indicated in sketch (d). (The exact motion of the flexible tip is immaterial, provided the surface is sufficiently smooth and its slope remains small.) After the solution has been found, the flexible extension is again imagined to

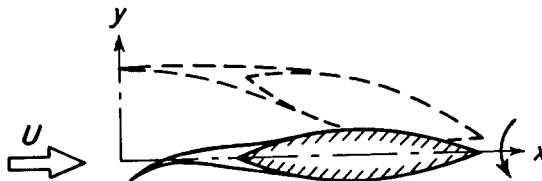


Sketch (c).- Steady flow past a smoothed wedge.



Sketch (d).- Smoothing for airfoil oscillating about leading edge.

shrink away, and the correct result is recovered for the actual airfoil oscillating about its nose.



Sketch (e).- Smoothing for airfoil oscillating about arbitrary point.

Finally, consider rotation about an arbitrary point. The flexible extension must now oscillate in such a way that its tip is always directed into the relative wind. Hence, as indicated in sketch (e), the tip must lie parallel with the free stream at the top (and bottom) of each stroke but incline in the direction of motion for intermediate positions.

We are accordingly led to consider the motion of an arbitrary flexible oscillating surface described by

$$y = \epsilon g(x) - \alpha_0 e^{i\omega t} h(x) \quad (16a)$$

where for the smoothed problem the functions $g(x)$ and $h(x)$ have continuous first derivatives. The smoothed problem will ultimately be replaced by the actual problem. According to comparison with equation (3b), this means that the function $h(x)$ will eventually be identified with $(x - b)$. The requirement that the leading edge of the smoothed shape be always parallel to the relative wind may be written as

$$\left. \begin{array}{l} g'(0) = 0 \\ h'(0) = iwb/U \end{array} \right\} \quad (16b)$$

(These last conditions, as well as the requirement that $g'(x)$ be continuous, must be relaxed in recovering the solution of the actual problem.)

Boundary Conditions

The boundary condition at the surface of the airfoil is that the normal component of velocity is zero. For any surface described by $S(x, y, t) = 0$ moving through a velocity field \vec{q} , this condition means that the substantial derivative of S (i.e., its time rate of change for an observer moving with the fluid) vanishes at the surface (see ref. 6), so that

$$S_t + \vec{q} \cdot \nabla S = 0 \quad \text{at } S = 0 \quad (17)$$

With velocity components given in terms of Φ by equation (9b), and for the smoothed surface described by equation (16a), this tangency condition becomes

$$\Phi_y = (1 + \Phi_x)(\epsilon g' - \alpha_0 e^{i\omega t} h') - \frac{i\omega}{U} \alpha_0 e^{i\omega t} h \quad \text{at } y = \epsilon g - \alpha_0 e^{i\omega t} h \quad (18)$$

where $g \equiv g(x)$, etc. It is convenient to refer this condition to the axis $y = 0$ by expanding in Taylor series. Keeping only terms of second order gives

$$\Phi_y = (1 + \Phi_x)(\epsilon g' - \alpha_0 e^{i\omega t} h') - \frac{i\omega}{U} \alpha_0 e^{i\omega t} h - (\epsilon g - \alpha_0 e^{i\omega t} h) \Phi_{yy}$$

at $y = 0 \quad (19)$

(Here Φ_x and Φ_{yy} on the right-hand side can be evaluated from linearized theory.)

The upstream boundary condition requires that in the actual problem, the Rankine-Hugoniot relations (or at least a simplified second-order form thereof) be satisfied across an oscillating bow shock wave whose position must be determined. However, shock waves have been eliminated from the smoothed problem, so that it is only necessary to require that the perturbation potential Φ vanish along the oscillating characteristic line (Mach line) springing from the leading edge. This insures that all disturbances produced by the airfoil are swept downstream. An equivalent and still simpler requirement is that Φ and its streamwise derivative vanish on, say, the plane $x = 0$:

$$\Phi = \Phi_x = 0 \quad \text{at } x = 0 \quad (20)$$

Restriction to Small Angles of Attack

It is convenient to seek a solution to second order in the airfoil thickness, but to only first order in angle of attack. This is not a serious limitation because, just as in steady flow, second-order terms in angle of attack, though affecting local pressures, have no effect upon lift or moment because they are equal on the upper and lower surfaces.

As a consequence of this restriction to linear terms in angle of attack, the awkward question of when the bow shock wave detaches will not arise. The amplitude of oscillation may be regarded as infinitesimal, so that if the bow shock is attached in the mean steady flow, it will remain so during the oscillation.

Transformation of Perturbation Equation

It is convenient to separate the time-dependent part of the problem from the mean steady flow at zero angle of attack (for which the second-order solution is known). Furthermore, for harmonic oscillations the number of independent variables is then reduced to two by separating an exponential time factor. Finally, the linear portion of the time-dependent equation is reduced to normal form by a transformation of dependent variable. These three transformations amount to setting

$$\Phi(x, y, t) = \phi(x, y) + \alpha_0 e^{i(\omega t - \kappa x)} \Psi(x, y) \quad (21a)$$

where

$$\kappa = \frac{M^2}{\beta^2} \frac{\omega}{U} \quad (21b)$$

Here ϕ corresponds to the mean steady flow, and the term in Ψ represents the additional flow associated with the oscillation through small angle of attack.¹

Introducing this transformation into the perturbation equation (eq. (11)) gives for

$$\phi_{yy} - \beta^2 \phi_{xx} = M^2 \left[(\gamma-1) \phi_x \Delta \phi + (\phi_x^2 + \phi_y^2)_x \right] \quad (22)$$

where Δ is the Laplacian operation $\partial^2/\partial x^2 + \partial^2/\partial y^2$, and for Ψ

$$\Psi_{yy} - \beta^2 \Psi_{xx} - \left(\frac{\beta \kappa}{M} \right)^2 \Psi =$$

$$\begin{aligned} & M^2 \left[(\gamma-1) (\phi_x \Delta \Psi + \Psi_x \Delta \phi) + 2(\phi_x \Psi_x + \phi_y \Psi_y)_x \right] - i\kappa M^2 \left[(\gamma-1) (2\phi_x \Psi_x + \frac{1}{M^2} \Psi \Delta \phi) + \right. \\ & \left. 2 \left(\frac{M^2 + 1}{M^2} \phi_x \Psi_x + \phi_{xx} \Psi + \frac{1}{M^2} \phi_y \Psi_y \right) \right] - \kappa^2 \left[2 + (\gamma-1) M^2 \right] \phi_x \Psi \end{aligned} \quad (23)$$

¹If second-order terms in angle of attack were retained, equation (21a) would include also a term $\alpha_0^2 e^{2i(\omega t - \kappa x)} \chi(x, y)$, which would appear only in the second-order solution. The differential equation for χ would have the form

$$\chi_{yy} - \beta^2 \chi_{xx} - \left(\frac{2\beta\kappa}{M} \right)^2 \chi = M^2 \left[(\gamma-1) \Psi_x \Delta \Psi + \dots \right]$$

and could be solved just as is the equation for Ψ .

The tangency condition of equation (19) likewise separates into the two conditions

$$\phi_y = \epsilon(1 + \phi_x)g' - \epsilon \phi_{yy} g \quad \text{at } y = 0 \quad (24)$$

$$\begin{aligned} \Psi_y &= -e^{ikx}(1 + \phi_x)h' - ik \frac{\beta^2}{M^2} e^{ikx} h + \epsilon(\Psi_x - ik\Psi)g' - \\ &\quad \epsilon \Psi_{yy} g + e^{ikx} \phi_{yy} h \quad \text{at } y = 0 \end{aligned} \quad (25)$$

For the actual problem the second of these becomes, identifying $h(x)$ with $(x - b)$,

$$\begin{aligned} \Psi_y &= -e^{ikx}(1 + \phi_x) - ik \frac{\beta^2}{M^2} e^{ikx}(x - b) + \epsilon(\Psi_x - ik\Psi)g' - \\ &\quad \epsilon \Psi_{yy} g + e^{ikx} \phi_{yy}(x - b) \quad \text{at } y = 0 \end{aligned} \quad (26)$$

For pressures at the surface of the airfoil, the relation of equation (14) can be expressed in terms of values at $y = 0$ by Taylor series expansion, with the result that to second order in thickness and first order in angle of attack

$$\begin{aligned} C_{p_u} &= (-2\phi_x - 2\epsilon\phi_{xy}g + \beta^2\phi_x^2 - \phi_y^2) + \\ &\quad 2a_0 e^{i(\omega t - kx)} \left[\frac{ik}{M^2} \Psi - \Psi_x + \epsilon \left(\frac{ik}{M^2} \Psi_y - \Psi_{xy} \right) g + \right. \\ &\quad \left. \beta^2 \phi_x \Psi_x - \phi_y \Psi_y + e^{ikx} \phi_{xy} h \right] \end{aligned} \quad (27)$$

Solution by Iteration

Although the equation for ϕ is nonlinear, that for Ψ is linear, but with nonconstant coefficients depending upon ϕ . This corresponds to the physical concept that because of the restriction to linear terms in angle of attack, the oscillatory part of the flow is an acoustic field with, however, the speed of sound varying from point to point in accordance with the mean steady flow.

The well-known linearized or first-order theory results from disregarding the right-hand sides of equations (22) and (23). Thus, with the

first-order potentials denoted by the lower case letters ϕ and ψ , the perturbation equations become

$$\phi_{yy} - \beta^2 \phi_{xx} = 0 \quad (28)$$

$$\psi_{yy} - \beta^2 \psi_{xx} - \left(\frac{\beta\kappa}{M}\right)^2 \psi = 0 \quad (29)$$

The second-order solution is obtained by iterating upon the first-order results. Using the linear equations to simplify the right-hand sides gives for the second-order iteration equations

$$\phi_{yy} - \beta^2 \phi_{xx} = 2M^2 [\beta^2 (N - 1) \phi_x^2 + \phi_y^2]_x \quad (30)$$

and

$$\begin{aligned} \psi_{yy} - \beta^2 \psi_{xx} - \left(\frac{\beta\kappa}{M}\right)^2 \psi &= 2M^2 [\beta^2 (N - 1) \phi_x \psi_x + \phi_y \psi_y]_x - \\ &2ik [\beta^2 (2N - 1) \phi_x \psi_x + \beta^2 N \phi_{xx} \psi + \phi_y \psi_y] - 2N \left(\frac{\beta\kappa}{M}\right)_{\phi=\psi}^2 \end{aligned} \quad (31)$$

where

$$N = \frac{\gamma + 1}{2} \frac{M^2}{\beta^2} \quad (32)$$

(Here, following the usual subscript notation for derivatives, $[\phi_y^2]_x$ means $\partial \phi_y^2 / \partial x$, etc.) The second-order solution for ϕ , which leads to Busemann's well-known result at the airfoil surface (ref. 1), was given in reference 5. It is therefore necessary to consider only the second-order problem for ψ . Details of the iteration procedure and discussion of its limitations are given for the steady flow in reference 5 and apply also to the present problem.

Partial Particular Integral

The solution of the differential equation for steady flow in reference 5 was simplified by discovery of a particular integral of the iteration equation in terms of the first-order solution. It was also shown there that for steady three-dimensional flow, a particular integral can be found to account for all terms in the iteration equation except those involving the adiabatic exponent γ in the form of N . Likewise,

here, a partial particular integral which accounts for all terms on the right-hand side of equation (31) except those involving N is given by

$$\Psi^* = M^2 (\varphi \psi)_x - i\kappa \varphi \psi \quad (33)$$

The complete solution is this partial particular integral plus a solution of the reduced equation whose right-hand side contains only the terms still unaccounted for:

$$\Psi_{yy} - \beta^2 \Psi_{xx} - \left(\frac{\beta \kappa}{M}\right)^2 \Psi = 2\beta^2 N \left\{ M^2 (\varphi_x \psi_x)_x - i\kappa [(\varphi_x \psi)_x + \varphi_x \psi_x] - \frac{\kappa^2}{M^2} \varphi_x \psi \right\} \quad (34)$$

First-Order Solution

The first-order solution for φ is known from Ackeret's theory to be

$$\varphi = -\frac{\epsilon}{\beta} g(x - \beta y) \quad (35)$$

It is to be understood here and in all similar expressions to follow that this is the potential only for $x \geq \beta y$, and that φ vanishes identically ahead of the bow Mach wave (where $x \leq \beta y$).

The first-order equation for ψ (eq. (29)) is most readily solved by applying the Laplace transformation with respect to x . We denote the Laplace transform of a function either by a bar, or by the symbol L , whichever is more convenient (and the inverse transform by L^{-1}), so that

$$\left. \begin{array}{l} \bar{f}(s) \\ L\{f(x)\} \end{array} \right\} = \int_0^\infty e^{-sx} f(x) dx \quad (36)$$

Applying this transformation to equation (29), using the fact that ψ and ψ_x vanish at $x = 0$, gives

$$\bar{\Psi}_{yy} - \beta^2 \left(s^2 + \frac{\kappa^2}{M^2} \right) \bar{\Psi} = 0 \quad (37)$$

The solution of this equation which represents waves moving downstream is

$$\bar{\psi} = C(s) e^{-\beta y} \sqrt{s^2 + \kappa^2/M^2} \quad (38)$$

The constant $C(s)$ is determined by the first-order form of the tangency condition (eq. (25)), which transforms to

$$\bar{\psi}_y = -\bar{w}(s) \quad \text{at } y = 0 \quad (39a)$$

where

$$w(x) = e^{ikx} \left[h'(x) + ik \frac{\beta^2}{M^2} h(x) \right] \quad (39b)$$

is the downwash velocity at $y = 0$.

Consequently,

$$\bar{\psi} = \frac{1}{\beta} \bar{w}(s) \frac{e^{-\beta y} \sqrt{s^2 + \kappa^2/M^2}}{\sqrt{s^2 + \kappa^2/M^2}} \quad (40)$$

The inverse transformation is readily carried out using the standard tables (e.g., ref. 7) together with the convolution theorem, which gives as the solution of the smoothed problem

$$\psi(x, y) = \frac{1}{\beta} \int_0^{x-\beta y} J_0 \left(\frac{\kappa}{M} \sqrt{\xi^2 - \beta^2 y^2} \right) w(x - \xi) d\xi \quad (41)$$

The solution for the actual problem is now obtained by setting $h(x) = x - b$, which gives finally²

$$\psi(x, y) = \frac{1}{\beta} \int_0^{x-\beta y} J_0 \left(\frac{\kappa}{M} \sqrt{\xi^2 - \beta^2 y^2} \right) e^{ik(x-\xi)} \left[1 + ik \frac{\beta^2}{M^2} (x - \xi - b) \right] d\xi \quad (42)$$

in agreement with the known result of linearized theory (see, e.g., ref. 8).

²The smoothing was, of course, unnecessary in this first-order problem.

SECOND-ORDER SOLUTION FOR LOW FREQUENCIES

Because the first-order solution for arbitrary frequencies is rather complicated, use is sometimes found for an expansion in powers of frequency, which involves only elementary functions. The corresponding second-order solution will now be carried out in detail, including linear terms in frequency. This result will serve, for example, to evaluate the effects of thickness upon one-degree-of-freedom torsional instability, which is primarily a low-frequency effect. Thereafter, the result of extending the solution to include third powers of frequency will simply be stated.

Potential Including Linear Terms in Frequency

Expanding the first-order solution of equation (41) in powers of the frequency parameter κ and retaining only linear terms gives

$$\psi(x, y) = \frac{1}{\beta} \int_0^z w(\xi) d\xi + \dots O(\kappa^2) = \psi(z) + \dots \quad (43)$$

where $z = x - \beta y$. To this order the partial particular integral of equation (33) is a solution of the homogeneous equation (eq. (29)), and can therefore be disregarded. Substituting the first-order solutions into the right-hand side of equation (34) and applying the Laplace transformation gives, to order κ ,

$$\bar{\Psi}_{yy} - \beta^2 s^2 \bar{\Psi} = -2\epsilon N e^{-\beta sy} \left[(M^2 s - ik) L \left\{ g'(x) \psi'(x) \right\} - ik s L \left\{ g'(x) \psi(x) \right\} \right] \quad (44)$$

It is readily found that a particular integral of this equation is given by an appropriate multiple of $y e^{-\beta sy}$. Then, adding a complementary function representing downgoing waves gives

$$\bar{\Psi} = C(s) e^{-\beta sy} + \frac{\epsilon N}{\beta} y e^{-\beta sy} \left[\left(M^2 - \frac{ik}{s} \right) L \left\{ g' \psi' \right\} - ik L \left\{ g' \psi \right\} \right] \quad (45)$$

where the constant C is to be evaluated from the tangency condition. Inverting the Laplace transformation shows that for the actual problem, in which $h(x) = x - b$, the solution has the form

$$\Psi = f(z) + \frac{\epsilon N}{\beta} y \left[M^2 g' + ik (2\beta^2 z g' - \beta^2 b g' - g) \right] \quad (46a)$$

where $g \equiv g(z)$. The arbitrary function $f(z)$ is determined from the tangency condition of equation (26) to be

$$f(z) = \frac{z}{\beta} + \frac{i\kappa}{\beta} z \left(\frac{2M^2-1}{2M^2} z - \frac{\beta^2}{M^2} b \right) + \epsilon \left[\frac{M^2 N - M^2 - 1}{\beta^2} g + (x-b) g' \right] + \\ i\kappa \epsilon \left\{ \left[2 - (N-1) \frac{2M^2-1}{\beta^2} \right] \int_0^z g(\xi) d\xi + \left[2(N-1) - \frac{2M^2-1}{M^2 \beta^2} \right] zg + z(z-b)g' + \right. \\ \left. \left[\frac{1}{M^2} - (N-1) \right] bg \right\} \quad (46b)$$

Surface Pressure Coefficient

The pressure coefficient at the upper surface of the actual airfoil is found from equation (27) to be

$$C_{p_u} = C_{p_0} + 2\alpha_0 e^{i\omega t} \left\{ -\frac{1}{\beta} + i\kappa \frac{\beta}{M^2} \left(b + \frac{2-M^2}{\beta^2} x \right) - \frac{M^2 N - 2}{\beta^2} \epsilon g' + \right. \\ \left. i\kappa \frac{\epsilon}{M^2} \left[2M^2 \frac{N-1}{\beta^2} g + \frac{(2-M^2)(M^2 N - 1)}{\beta^2} x g' + (M^2 N - 2)bg' \right] \right\} + \\ \dots O(\kappa^2, \epsilon^2 \alpha, \alpha^2) \quad (47)$$

where $g \equiv g(x)$. Here C_{p_0} is the value for the mean steady flow (at zero angle of attack) which is given by Busemann's second-order theory. A more useful form of the result is obtained by extracting the real part and expressing the result in terms of the instantaneous angle of attack $\alpha(t)$ and its time rate of change $\dot{\alpha}(t)$. Furthermore, the parameter ϵ has served its purpose of distinguishing terms of different orders and can be eliminated (according to eq. (1)). Thus, on the upper surface of an arbitrary airfoil which is described at zero angle of attack by $y = Y(x)$, is pivoted about a point a distance b downstream of its leading edge, and performs slow angular oscillations described by $\alpha(t)$, the pressure coefficient is, to second order in thickness and first order in angle of attack,

$$C_{p_u} = C_{p_0} - \frac{2}{\beta} \alpha + \frac{2}{\beta} \left(\frac{2-M^2}{\beta^2} x + b \right) \frac{\dot{\alpha}}{U} - 2 \frac{M^2 N - 2}{\beta^2} Y' \alpha + \\ 2 \left[\frac{2M^2(N-1)}{\beta^4} Y + \frac{(2-M^2)(M^2 N - 1)}{\beta^4} x Y' + \frac{M^2 N - 2}{\beta^2} b Y' \right] \frac{\dot{\alpha}}{U} + \dots O(\ddot{\alpha}, \epsilon^2 \alpha, \alpha^2) \quad (48a)$$

Here the value for the mean steady flow is (ref. 1)

$$C_{p_0} = \frac{2}{\beta} Y' + \frac{M^2 N - 2}{\beta^2} Y'^2 \quad (48b)$$

(A preliminary report of this result was given in ref. 9.) In this form, the result is not restricted to sinusoidal motion but applies to any oscillation which is sufficiently smooth and slow that the pressures depend significantly only upon the instantaneous angle of attack and angular velocity.

The pressure on the lower surface of the airfoil is obtained from these equations by reversing the sign of α , and taking $Y(x)$ to be the ordinate of the lower surface, measured positive downward.

The result for plunging motions can be extracted by letting α tend to zero and b tend to infinity in such a way that their product remains finite, say

$$b\alpha(t) = h(t) \quad (49)$$

In the limit, the airfoil simply translates vertically according to $y = h(t)$. The pressure coefficient on the upper surface is³

$$C_{p_u} = C_{p_0} + \frac{2}{\beta} \frac{\dot{h}}{U} + 2 \frac{M^2 N - 2}{\beta^2} Y' \frac{\dot{h}}{U} \quad (50)$$

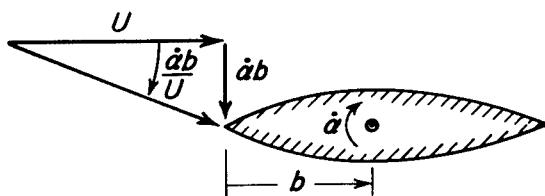
Checks on the Result

The solution can be tested in several special cases for which the result can be derived from other considerations.

³Note that, as it should be, this is just the result of using Busemann's formula for steady flow (eq. (48b)), with the local slope increased by the instantaneous apparent downwash angle \dot{h}/U ; see the discussion in the following section of conditions at the nose.

Of the five terms in equation (48a), the first is known from Busemann's steady second-order solution, and the second and third from linearized unsteady theory. The fourth is obtained by using the instantaneous airfoil slope ($Y' - \alpha$) instead of the mean steady slope Y' in Busemann's formula and retaining only linear terms in α . Therefore, only the last term, which is the essentially new result of the present analysis, requires verification.

Just at the nose of an oscillating airfoil, the pressure can be determined exactly if the bow shock wave is attached. The transition through the moving bow shock is instantaneous, and so depends only upon the relative velocity at that instant (see ref. 4, p. 297). Hence the pressure just at the nose is instantaneously the same as on a wedge of the same vertex angle in steady flow with the same relative velocity.

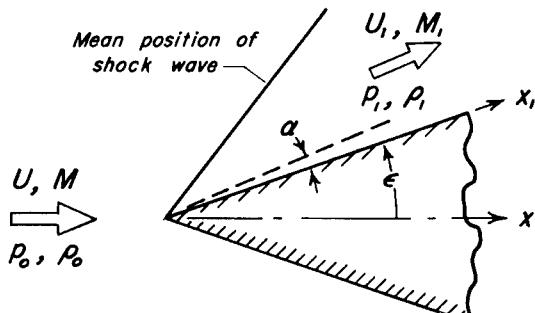


Sketch (f).- Velocity relative to leading edge of oscillating airfoil.

angle $\dot{\alpha}b/U$. Replacing Y' by $Y' + \dot{\alpha}b/U$ in Busemann's formula (eq. (48b)) gives, to first order in angle of attack

$$C_{p_u} = C_{p_0} + \frac{2}{\beta} b \frac{\dot{\alpha}}{U} + 2 \frac{M^2 N - 2}{\beta^2} b Y' \frac{\dot{\alpha}}{U} \quad (51)$$

which checks the part proportional to b of the last term in equation (48a).



Sketch (g).- Wedge oscillating about its vertex.

The remainder of the term in question can be checked for a single-wedge airfoil oscillating about its vertex (sketch (g)). It can be shown using the results of reference 3 that in this case disturbances reflected from the shock wave are of third order in the wedge angle (although for other pivot positions they are of second order). Therefore, a solution correct to second order in thickness and first order

in angle of attack can be found by applying linearized theory to the mean steady flow behind the shock wave.⁴ For slow oscillations, the first three terms of equation (48a) give

$$\frac{p-p_1}{\frac{1}{2}\rho_1 U_1^2} = -\frac{2}{\beta_1} \alpha + \frac{2(2-M_1^2)}{\beta_1^3} x_1 \frac{\dot{\alpha}}{U_1} \quad (52)$$

where subscript 1 denotes values in the mean steady flow behind the shock wave. From linearized theory

$$\left. \begin{aligned} M_1 &= M \left[1 - \beta (N-1) \epsilon \right] \\ \beta_1 &= \beta \left[1 - \frac{M^2}{\beta} (N-1) \epsilon \right] \\ U_1 &= U \left[1 - \frac{\epsilon}{\beta} \right] \\ p_1 &= p_0 \left[1 + \gamma \frac{M^2}{\beta} \epsilon \right] \\ \rho_1 &= \rho_0 \left[1 + \frac{M^2}{\beta} \epsilon \right] \end{aligned} \right\} \quad (53)$$

where ϵ is the semivertex angle. Hence, referring the surface pressure coefficient to free-stream quantities (and noting that $x_1 = x$ to second order) gives

$$\begin{aligned} C_{p_u} &= C_{p_0} - \frac{2}{\beta} \alpha + 2 \frac{2-M^2}{\beta^3} x \frac{\dot{\alpha}}{U} - 2 \frac{M^2 N - 2}{\beta^2} \epsilon \alpha + \\ &\quad 2 \frac{2M^2(N-1) + (2-M^2)(M^2 N - 1)}{\beta^4} \epsilon x \frac{\dot{\alpha}}{U} \end{aligned} \quad (54)$$

which checks the first two parts of the last term in equation (48a) when $Y(x) = \epsilon x$.

Recently, Lighthill has given a further check for the case of Mach numbers so high that $1/M^2$ is negligible compared with unity (ref. 10).

⁴This concept was suggested to the author by W. P. Jones of the National Physical Laboratory, England.

Lift and Moment Coefficients for Symmetrical Airfoils

The coefficients of lift and pitching moment (about the pivot) are given in terms of the pressure coefficients on the upper and lower surfaces by

$$c_l = \frac{1}{c} \int_0^c (c_{p_l} - c_{p_u}) dx \quad (55a)$$

$$c_m = \frac{1}{c^2} \int_0^c (b - x)(c_{p_l} - c_{p_u}) dx \quad (55b)$$

For simplicity, consider only airfoils symmetric about the chord line. In this case, the pressure difference is given by

$$\begin{aligned} c_{p_l} - c_{p_u} = & \frac{4}{\beta} \alpha - \frac{4}{\beta} \left(\frac{2-M^2}{\beta^2} x + b \right) \frac{\dot{\alpha}}{U} + 4 \frac{M^2 N - 2}{\beta^2} Y' \alpha - \\ & 4 \left[\frac{2M^2(N-1)}{\beta^4} Y + \frac{(2-M^2)(M^2 N - 1)}{\beta^4} xY' + \frac{M^2 N - 2}{\beta^2} bY' \right] \frac{\dot{\alpha}}{U} \end{aligned} \quad (56)$$

If the airfoil has a sharp trailing edge, substituting into equations (55) and integrating by parts gives

$$c_l = \frac{4}{\beta} \alpha - \frac{4}{\beta} \left[\left(\frac{2-M^2}{2\beta^2} + \frac{b}{c} \right) + \frac{M^4 N - 3M^2 + 2}{\beta^3} \frac{1}{c^2} \int_0^c Y dx \right] \frac{c \dot{\alpha}}{U} \quad (57)$$

and

$$\begin{aligned} c_m = & \frac{4}{\beta} \left[\left(\frac{b}{c} - \frac{1}{2} \right) + \frac{M^2 N - 2}{\beta} \frac{1}{c^2} \int_0^c Y dx \right] \alpha + \frac{4}{\beta} \left[\left(\frac{2-M^2}{3\beta^2} + \frac{2M^2 - 3}{2\beta^2} \frac{b}{c} - \frac{b^2}{c^2} \right) - \right. \\ & \left. \frac{M^2(N-1)}{\beta^3} \frac{b}{c} \frac{1}{c^2} \int_0^c Y dx + 2 \frac{M^2 N - 2}{\beta} \frac{1}{c^3} \int_0^c (x-b) Y dx \right] \frac{c \dot{\alpha}}{U} \end{aligned} \quad (58)$$

Inside each square bracket the first term is the result of linearized theory, and the remainder represents the second-order effect of thickness. Thickness effects are seen to appear in the form of the area of the airfoil profile and its first moment about the vertical line through the pivot.

If the airfoil has a blunt trailing edge of semithickness $Y(c)$, the following additional second-order terms must be added to the above expressions:

to c_l :

$$\frac{4}{\beta} \frac{M^2 N - 2}{\beta} \frac{Y(c)}{c} \alpha - \frac{4}{\beta} \left[\frac{M^2 N - 2}{\beta} \frac{b}{c} + \frac{(2-M^2)(M^2 N - 1)}{\beta^3} \right] \frac{Y(c)}{c} \frac{c \dot{\alpha}}{U} \quad (59)$$

to c_m :

$$- \frac{4}{\beta} \frac{M^2 N - 2}{\beta} \left(1 - \frac{b}{c} \right) \frac{Y(c)}{c} \alpha + \frac{4}{\beta} \left[\frac{M^2(N-1)}{\beta^3} - \frac{M^2 N - 2}{\beta} \left(1 - \frac{b}{c} \right) \right] \left(1 - \frac{b}{c} \right) \frac{Y(c)}{c} \frac{c \dot{\alpha}}{U} \quad (60)$$

Examples: Biconvex and Double-Wedge Airfoils

To second order, a biconvex airfoil of thickness ratio τ is given by the parabolas

$$y = \pm Y(x), \quad Y(x) = 2\tau \frac{x}{c} (c-x) \quad (61)$$

The expressions for lift and moment become

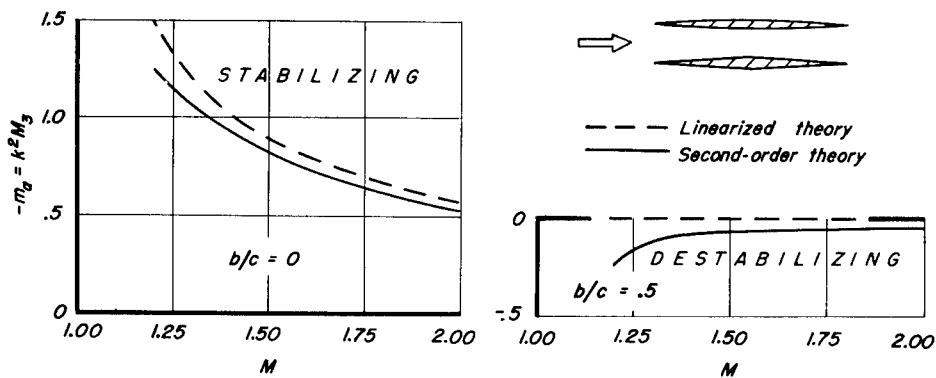
$$c_l = \frac{4}{\beta} \alpha - \frac{4}{\beta} \left[\left(\frac{2-M^2}{2\beta^2} + \frac{b}{c} \right) + \frac{M^4 N - 3M^2 + 2}{3\beta^3} \tau \right] \frac{c \dot{\alpha}}{U} \quad (62)$$

$$c_m = \frac{4}{\beta} \left[\left(\frac{b}{c} - \frac{1}{2} \right) + \frac{M^2 N - 2}{3\beta} \tau \right] \alpha + \frac{4}{\beta} \left[\left(\frac{2-M^2}{3\beta^2} + \frac{2M^2 - 3}{2\beta^2} \frac{b}{c} - \frac{b^2}{c^2} \right) + \frac{M^2 N - 2}{3\beta} \left(1 - 2 \frac{b}{c} \right) \tau - M^2 \frac{N-1}{3\beta^3} \frac{b}{c} \tau \right] \frac{c \dot{\alpha}}{U} \quad (63)$$

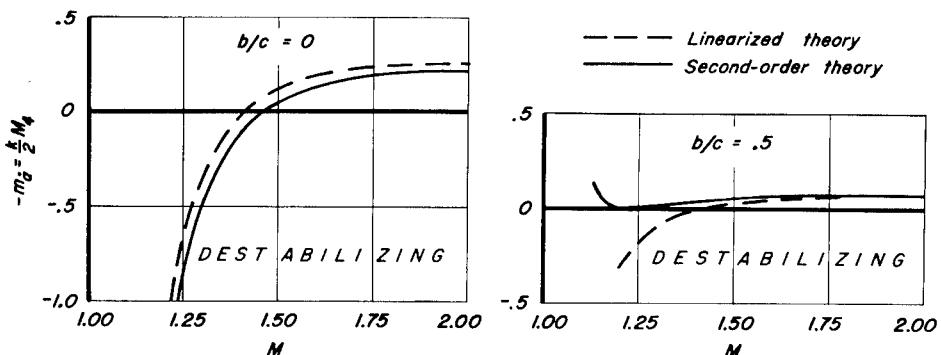
It happens that for a double-wedge airfoil (with maximum thickness at midchord), both the area and first moment are just three fourths of those for the biconvex airfoil. Consequently, the above results apply to double-wedge airfoils, if $\tau/3$ is replaced throughout by $\tau/4$.

In the expression for pitching moment, the term proportional to α represents an aerodynamic stiffness or restoring moment in phase with the angular displacement, while the term proportional to $\dot{\alpha}$ corresponds to an aerodynamic damping moment in phase with the angular velocity. The effects of thickness upon aerodynamic restoring and damping moments

are shown in sketches (h) and (i) for a 6-percent-thick double-wedge or a 4-1/2-percent-thick biconvex airfoil with two different pivot positions. The sketches have been labelled with both the usual American notation (e.g., ref. 11) and the British notation (e.g., ref. 12),



Sketch (h).- Effect of thickness upon restoring moment coefficient for 4-1/2-percent-thick biconvex or 6-percent-thick double-wedge airfoil.



Sketch (i).- Effect of thickness upon damping moment coefficient for 4-1/2-percent-thick biconvex or 6-percent thick double-wedge airfoil.

defined for harmonic oscillations of arbitrary frequency by

$$\frac{c_m}{4\alpha_0 e^{i\omega t}} = \left\{ \begin{array}{ll} -\frac{1}{2} k^2 (M_3 + iM_4) & (\text{American}) \\ \frac{1}{2} (m_\alpha + i\lambda m_\alpha) & (\text{British}) \end{array} \right\} \quad (64)$$

Here k and λ are the reduced frequency in the American and British notations, respectively, related by

$$\lambda = 2k = \frac{\omega c}{U} \quad (65)$$

For slow oscillations, the coefficients are given by

$$\left. \begin{aligned} m_\alpha &= -k^2 M_3 = \frac{1}{2} \frac{\partial c_m}{\partial \alpha} \\ m_{\dot{\alpha}} &= -\frac{k}{2} M_4 = \frac{U}{2c} \frac{\partial c_m}{\partial \dot{\alpha}} \end{aligned} \right\} \quad (66)$$

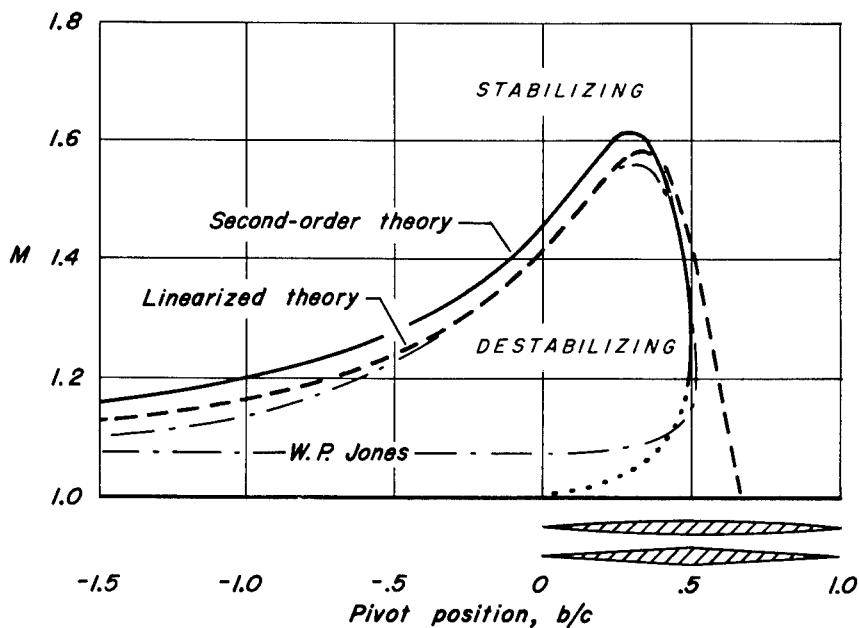
(and, indeed, this was originally the definition of m_α and $m_{\dot{\alpha}}$, that given by equation (64) being a later extension to the case of rapid harmonic oscillations).

It should be noted that according to second-order theory, the non-linear effects of thickness are themselves linear in thickness. This means, for example, that doubling the airfoil thickness ratio would double the distance between the linearized and second-order curves of sketches (h) and (i).

Neutral Damping Boundary

Linearized theory indicates the possibility of instability of pitching oscillations for low frequencies. For a range of Mach numbers below $\sqrt{5}/2 = 1.58$ and pivots ahead of two thirds of the chord, the aerodynamic damping moment becomes negative, and so tends to destabilize. (Whether or not the motion is actually unstable depends, of course, upon the other dynamic parameters in the problem.) This zone of possible instability shrinks and eventually disappears as the frequency of oscillation increases. The present low-frequency solution is therefore adequate for determining how the region of instability is modified by nonlinear thickness effects.

Sketch (j) shows the boundary of neutral aerodynamic damping for slow oscillations of a 4-1/2-percent-thick biconvex or 6-percent-thick double-wedge airfoil. The aerodynamic damping is destabilizing for Mach numbers and pivot positions lying inside the loops. Within the region where linearized theory predicts a destabilizing moment, thickness is seen to exert a further destabilizing effect except for pivots near midchord. The second-order solution becomes unreliable when the bow shock wave detaches, at about $M = 1.2$.



Sketch (j).- Neutral damping boundary for 4-1/2-percent-thick biconvex or 6-percent-thick double-wedge airfoil.

Comparison With Previous Investigations

Two previous investigators have sought a second-order solution for slowly oscillating airfoils in supersonic flow. Their results agree neither with each other nor with the present solution.

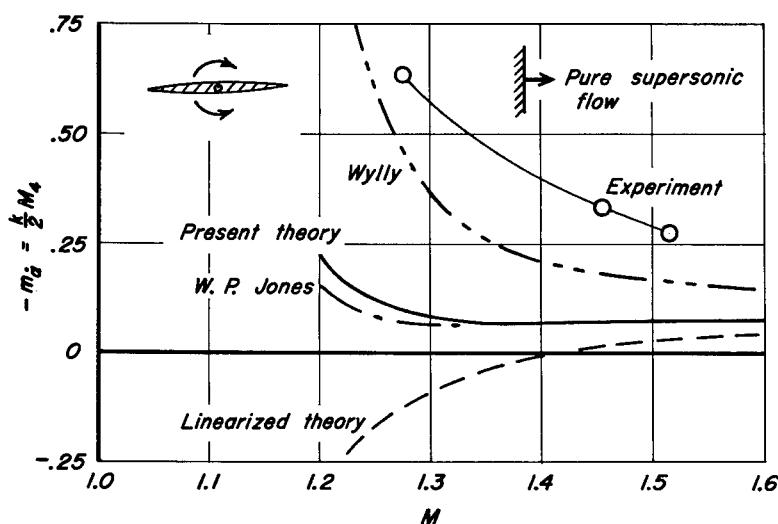
In 1947, W. P. Jones obtained an estimate of the thickness effect by assuming that the ratio of second-order to linearized pressure disturbances is the same for slow oscillations as that given by Busemann's formula for steady flow (ref. 13). That this assumption is not altogether correct is indicated by the fact that the results do not check those obtained for a wedge oscillating about its vertex by applying linearized theory to the mean steady flow behind the shock wave. However, the assumption is correct at the leading edge, and also (as noted by Lighthill in ref. 10) in the limit of high Mach number. It is seen in sketch (j) that this estimate fails to give a useful prediction of the actual effects of thickness, except for pivots near midchord.

In 1951, Alexander Wyllly attacked the problem by methods similar to those used here (ref. 14). Unfortunately, it appears that the smoothing was not carried out with sufficient care; as a consequence,

the solution satisfies none of the three checks discussed previously. In contrast to the present results, the effect of thickness upon aerodynamic damping was predicted to be stabilizing and so great that for airfoils of the thicknesses shown in sketch (j), the zone of possible instability would have disappeared altogether.

Comparison With Experiment

The only experimental results available are those quoted in reference 15, which are derived from tests by Bratt and Chinneck. A 7-1/2-percent-thick biconvex airfoil, pivoted at midchord, was tested at Mach numbers of 1.28, 1.46, and 1.52 over a range of frequency. The aerodynamic damping was measured by giving the airfoil an initial displacement and measuring the logarithmic decrement. The experimental data are shown in sketch (k) in comparison with linearized theory and



Sketch (k).- Comparison of experimental and theoretical damping moment coefficients for 7-1/2-percent-thick biconvex airfoil pivoted at midchord.

the second-order theories of W. P. Jones, Willy, and the present analysis. As indicated on the sketch, the lowest test Mach number lies in the range of mixed subsonic and supersonic flow (and a detached bow wave). The present theory predicts only a fraction of the discrepancy between experiment and linearized theory. The same is true of Jones' estimate which, according to sketch (j), agrees with the present analysis

only for pivots near midchord. Wylly's result, which has been shown to be erroneous, happens to lie much closer to the measured results.

Extension to Cube of Frequency

The dependence of thickness effects upon frequency of oscillation can be estimated by extending the second-order solution to include higher powers of frequency. This has been carried out for an arbitrary airfoil by including second and third powers, which is enough to show an effect of frequency upon both aerodynamic stiffness and damping. The computation, though cumbersome, is a straightforward extension of the previous analysis, so that only the final result will be given here.

The expression for pressure coefficient on the upper surface, corresponding to equation (47), is found to be

$$\begin{aligned}
 \frac{C_{pu} - C_{po}}{2\alpha_0 e^{i\omega t}} = & -\frac{1}{\beta} + \frac{i\kappa}{\beta} \left(\frac{2-M^2}{M^2} x + \frac{\beta^2}{M^2} b \right) + \frac{\kappa^2}{\beta} x \left(\frac{2+M^2}{4M^4} x + \frac{\beta^2}{M^4} b \right) - \\
 & \frac{i\kappa^3}{\beta} x^2 \left(\frac{M^2+4}{12M^4} x + \frac{3\beta^2}{4M^4} b \right) - \epsilon \frac{M^2 N - 2}{\beta^2} g' + \\
 & i\kappa \epsilon \left[2 \frac{N-1}{\beta^2} g + \frac{M^2 N - 2}{M^2} b g' + \frac{(2-M^2)(M^2 N - 1)}{M^2 \beta^2} x g' \right] + \\
 & \kappa^2 \epsilon \left[\frac{3(3M^2 - 2)N - 2(5M^2 - 3)}{2M^2 \beta^2} \int_0^x g + \frac{4N - 5}{2M^2} b g + \frac{(16 - 7M^2)N + 4(2M^2 - 3)}{4M^2 \beta^2} x g + \right. \\
 & \left. \frac{N-1}{M^2} b x g' + \frac{(2+M^2)N - 4}{4M^2 \beta^2} x^2 g' \right] + i\kappa^3 \epsilon \left[\frac{(17M^4 - 10M^2 - 4)N - (5M^2 - 2)(4M^2 - 1)}{2M^4 \beta^2} \int_0^x \xi g + \right. \\
 & \left. \frac{6M^2 - (5M^2 - 2)N}{2M^4} b \int_0^x g + \frac{7M^2(2M^2 - 1) - (12M^4 - 3M^2 - 4)N}{2M^4 \beta^2} x \int_0^x g + \right. \\
 & \left. \frac{2(M^2 + 1) - (M^2 + 8)N}{4M^4} b x g + \frac{(3M^2 + 2) - (3M^2 + 4)N}{4M^4 \beta^2} x^2 g + \right. \\
 & \left. \frac{2(M^2 + 1) - 3M^2 N}{4M^4} b x^2 g' + \frac{5M^2 + 2 - M^2(4 + M^2)N}{12M^4 \beta^2} x^3 g' \right] \quad (67)
 \end{aligned}$$

where $g \equiv g(x)$ and $\int_0^x g \equiv \int_0^x g(\xi) d\xi$, etc. (The first four terms are the result of linearized theory.) This result meets the three tests discussed previously, and also checks the solution given later for a

wedge with general pivot location at arbitrary frequency. The resulting expressions for lift and moment involve the airfoil thickness in the form of the area of the profile and its first three moments about the vertical line through the pivot.

Example: Biconvex Airfoil

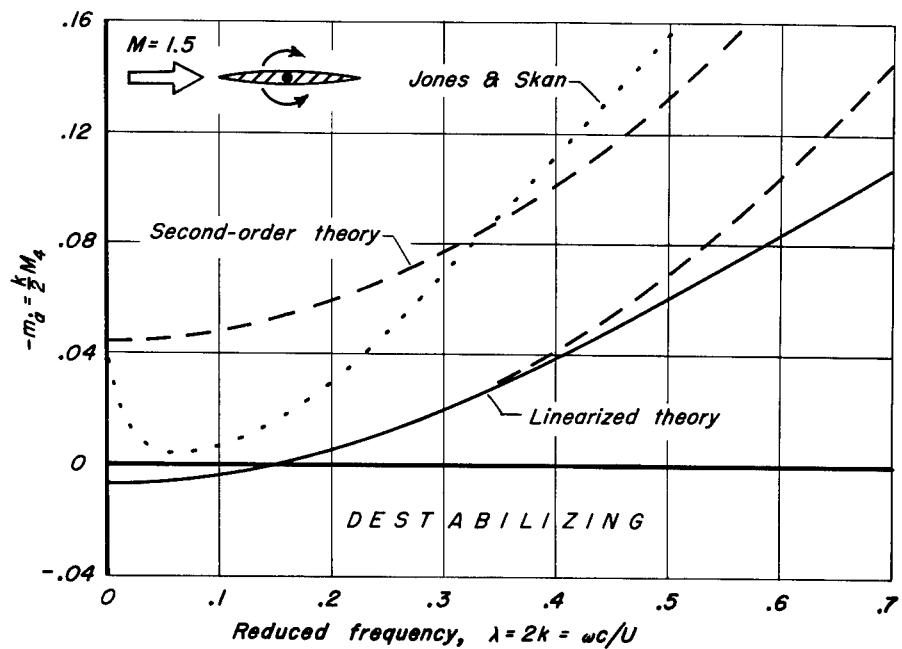
These rather formidable results simplify considerably for specific airfoils. For example, for a biconvex airfoil of thickness ratio τ oscillating about midchord, the pitching-moment coefficient is given by

$$\frac{C_m}{4\alpha_0 e^{i\omega t}} = i\lambda \frac{2-M^2}{12\beta^3} + \lambda^2 \frac{M^2}{16\beta^5} - i\lambda^3 \frac{M^2(6M^2-1)}{160\beta^7} + \tau \frac{M^2 N - 2}{3\beta^2} - i\lambda\tau \frac{M^2(N-1)}{6\beta^4} +$$

$$\lambda^2 \tau M^2 \frac{12(2-M^2)+(M^2-4)N}{240\beta^6} + i\lambda^3 \tau M^2 \frac{2(48M^4-61M^2+1)-(37M^4+25M^2-16)N}{1440\beta^8} \quad (68)$$

The first three terms are the result of linearized theory.

The component of this moment which is out of phase with the angle of attack gives a parabolic approximation for the variation of aerodynamic damping with frequency as shown by dashed lines in sketch (1)



Sketch (1).- Effect of frequency upon damping moment coefficient for 5-percent-thick biconvex airfoil pivoted at midchord.

for a 5-percent-thick biconvex airfoil. The accuracy of the parabolic approximation for linearized theory is indicated by comparing it with the exact result (solid line). In this example the linearized and second-order curves run almost parallel, which means that the nonlinear effects of thickness vary only slightly with frequency.

Recently, Jones and Skan have treated biconvex airfoils at arbitrary frequency by a numerical procedure (ref. 16). Their result is shown in sketch (l). It fails to give the initially parabolic form of the curve which is implied by the fact that the second-order solution, like the first-order result, can be expanded in powers of the square of the frequency. Their solution involves several doubtful assumptions, in particular, that the effect of the bow shock wave can be disregarded. It has already been remarked here that, actually, the bow shock has a second-order effect unless the pivot lies at the leading edge.

SECOND-ORDER SOLUTION FOR ARBITRARY FREQUENCIES

For some purposes the previous solution for slow oscillations may be inadequate. In principle, the second-order solution can be extended to include still higher powers of frequency, but the labor required is clearly prohibitive. Alternatively, one can attack directly the problem for arbitrary frequencies.

The second-order solution can, in fact, be carried out for a general airfoil at arbitrary frequencies. However, the result is formidable, involving multiple integrals of products of Bessel functions, and the reduction to simpler form for specific profiles appears to be difficult.

A more practical approach is to choose a specific airfoil shape in advance. Then the second-order solution involves only functions of the type encountered in the linearized theory. In particular, it is found that (at least for the simplest shape) the final expressions for lift and moment involve only functions which have been already studied and tabulated, so that numerical results are readily obtained.

Modified Smoothing Procedure

The smoothing discussed previously must be dropped at an earlier stage of the solution when a specific airfoil shape is chosen. It is therefore necessary first to modify the differential equation and boundary conditions so that no singular terms appear.

Consider first the differential equation (eq. (31)). Applying the Laplace transformation of equation (36), and envisioning the smoothed

problem, so that Ψ and Ψ_x vanish at $x = 0$, reduces it to

$$\bar{\Psi}_{yy} - \beta^2 \left(s^2 + \frac{k^2}{M^2} \right) \bar{\Psi} = 2(M^2 s - ik) \left[\beta^2(N-1)L\left\{\Phi_x \Psi_x\right\} + L\left\{\Phi_y \Psi_y\right\} - ik \frac{\beta^2 N}{M^2} L\left\{\Phi_x \Psi\right\} \right] \quad (69)$$

In this form, all troublesome second derivatives have disappeared from the right-hand side, so that the smoothing can now be dropped.

Consider next the tangency condition of equation (25), which contains second derivatives of both Φ and Ψ . These cause no difficulty when, as in the solution for slow oscillations, the tangency condition is imposed as it stands. However, its Laplace transform will be used here, and then the Dirac delta functions associated with the second derivatives would affect the integration implied in the inversion of the transformation. These troublesome second derivatives can be eliminated by first expressing them in terms of x derivatives only through the first-order equations:

$$\left. \begin{aligned} \Phi_{yy} &= \beta^2 \Phi_{xx} \\ \Psi_{yy} &= \beta^2 (\Psi_{xx} + \frac{k^2}{M^2} \Psi) \end{aligned} \right\} \quad (70)$$

and then applying the Laplace transformation while envisioning the smoothed problem (so that Φ , Ψ , Φ_x , and Ψ_x vanish at $x = 0$), which gives

$$\begin{aligned} \bar{\Psi}_y &= -\bar{w}(s) - M^2 L\left\{e^{ikx} \Phi_x\right\} + eM^2 L\left\{\Psi_x g'\right\} - ik\epsilon L\left\{\Psi g'\right\} - \beta^2 \epsilon s L\left\{\Psi_x g\right\} - \\ &\quad \beta^2 \epsilon \frac{k^2}{M^2} L\left\{\Psi g\right\} + \beta^2(s-ik) L\left\{e^{ikx} \Phi_x(x-b)\right\} \quad \text{at } y = 0 \end{aligned} \quad (71)$$

Again, all second derivatives have disappeared, so that the smoothing can be dropped.

Consider finally the upstream condition. For the smoothed problem, one statement of the condition was seen to be that the solution represents downgoing waves. This means that the complementary function for the iteration equation should have the same form as the linearized solution, and this statement of the upstream condition applies as well to the actual problem.

Solution for Wedge

The simple case of a single wedge illustrates the method of solution which can, in principle, be applied to any profile formed of piecewise analytic arcs. For a wedge of semivertex angle ϵ , the first-order solution for Φ is given by equation (35) as

$$\Phi = -\frac{\epsilon}{\beta} (x - \beta y) \quad (72)$$

and the first-order solution for ψ is given by equation (42). Substituting into the right-hand side of equation (69)⁵ gives for the transformed iteration equation

$$\bar{\Psi}_{yy} - \beta^2 \left(s^2 + \frac{\kappa^2}{M^2} \right) \bar{\Psi} = -2\epsilon(M^2 s - i\kappa) \left[1 + \frac{(N-1)s - i\kappa N/M^2}{\sqrt{s^2 + \kappa^2/M^2}} \right] \bar{w}(s) e^{-\beta y \sqrt{s^2 + \kappa^2/M^2}} \quad (73)$$

A particular integral of this equation is given by an appropriate multiple of $ye^{-\beta y \sqrt{s^2 + \kappa^2/M^2}}$, and adding a complementary function which represents downgoing waves gives the solution

$$\bar{\Psi} = C(s) e^{-\beta y \sqrt{s^2 + \kappa^2/M^2}} + \frac{\epsilon}{\beta} (M^2 s - i\kappa) \left[\frac{1}{\sqrt{s^2 + \kappa^2/M^2}} + \frac{(N-1)s - i\kappa N/M^2}{s^2 + \kappa^2/M^2} \right] \bar{w}(s) ye^{-\beta y \sqrt{s^2 + \kappa^2/M^2}} \quad (74)$$

The constant C is evaluated by imposing the tangency condition of equation (71), with the result that the Laplace transform of the second-order solution is found to be

$$\bar{\Psi} = \frac{e^{-\beta y \sqrt{s^2 + \kappa^2/M^2}}}{\beta \sqrt{s^2 + \kappa^2/M^2}} \left\{ \bar{w}(s) \left[1 + \epsilon y (M^2 s - i\kappa) + \frac{\epsilon}{\beta} (M^2 s - i\kappa) \frac{(N-1)s - i\kappa N/M^2}{\sqrt{s^2 + \kappa^2/M^2}} \left(\beta y + \frac{1}{\sqrt{s^2 + \kappa^2/M^2}} \right) \right] - \beta \epsilon \sqrt{s^2 + \kappa^2/M^2} \frac{d}{ds} \bar{w}(s) - \beta \epsilon b - \frac{\epsilon}{\beta} \frac{1}{s - i\kappa} \right\} \quad (75)$$

⁵In this simple case, the partial particular integral of equation (33) offers little actual simplification.

The inversion can be carried out using the standard tables (e.g., ref. 7) together with the convolution theorem. For calculating surface pressures, it suffices to obtain the solution in the plane $y = 0$, which is found to be

$$\begin{aligned} \Psi(x, 0) = & \frac{1}{\beta} \int_0^x J_0 \left(\frac{\kappa}{M} \xi \right) w(x-\xi) d\xi + \epsilon x w(x) + \\ & \epsilon \frac{M^2(N-1)}{\beta^2} x w(0) J_0 \left(\frac{\kappa}{M} x \right) - \epsilon b J_0 \left(\frac{\kappa}{M} x \right) + \\ & \frac{\epsilon}{\beta^2} \int_0^x J_0 \left(\frac{\kappa}{M} \xi \right) \left\{ \xi \left[M^2(N-1) w'(x-\xi) - i\kappa(2N-1)w(x-\xi) \right] - \right. \\ & \left. \kappa^2 \frac{N}{M^2} \int_0^{x-\xi} w(\eta) d\eta \right] - e^{i\kappa(x-\xi)} \right\} d\xi \end{aligned} \quad (76a)$$

where

$$w(x) = e^{i\kappa x} \left[1 + i\kappa \frac{\beta^2}{M^2} (x-b) \right] \quad (76b)$$

With the pivot at the nose ($b = 0$), this agrees with the result of applying linearized theory to the mean steady flow behind the shock wave. Also, when expanded in powers of frequency, it agrees with the previous low-frequency solution up to terms in κ^3 .

The surface pressure coefficient can now be calculated from equation (27) and the lift and moment coefficients from equations (55).

Example: Wedge Pivoted at Nose

For simplicity, the results will be given only for the special case of rotation about the nose. Then it is found that the lift and moment coefficients are given by

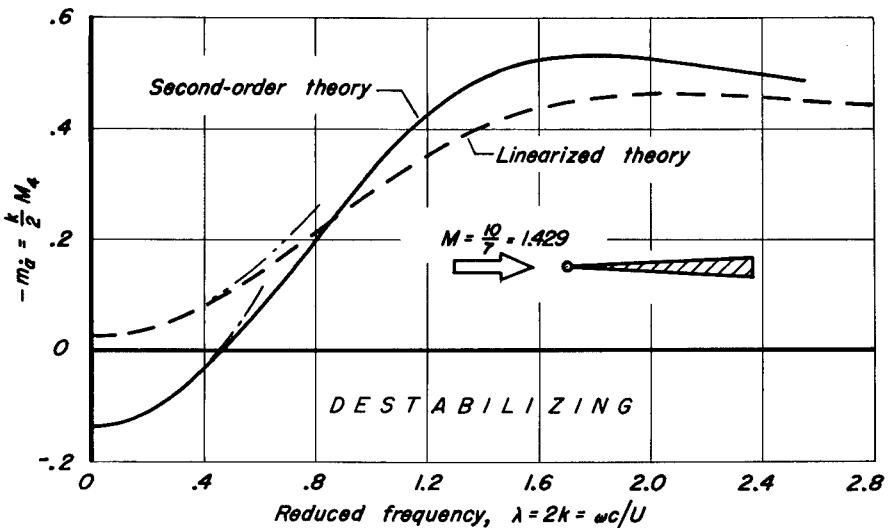
$$\begin{aligned}
 & \left. \frac{c_l}{4\alpha_0 e^{i\omega t}} \right\} = \left(\frac{1}{\beta} + \epsilon \frac{M^2 N - 2}{\beta^2} \right) f_{\nu} + (2-\nu) i\lambda \left(\frac{1}{\beta} + \epsilon \right) (f_0 - f_{1+\nu}) - \\
 & \quad \frac{\lambda^2}{2+\nu} \left(\frac{1}{\beta} + \frac{M^2}{\beta^2} \epsilon \right) (f_0 - f_{2+\nu}) + \\
 & \quad \frac{\lambda^2}{1+\nu} \left[\frac{1}{\beta} + \epsilon \left(4 \frac{M^2}{\beta^2} - \frac{3M^2+1}{M^2} N \right) \right] (f_1 - f_{2+\nu}) - \\
 & \quad \epsilon \frac{M^2}{\beta^2} \left(N-1 + \frac{N}{M^2} \right) \left[\left(1+\nu \right) f_{\nu} - e^{-i\lambda M^2/\beta^2} J_0 \left(M\lambda/\beta^2 \right) \right] - \\
 & \quad i\lambda \epsilon \left(3 \frac{M^2}{\beta^2} - \frac{3M^4 - M^2 - 1}{M^2 \beta^2} N \right) f_{1+\nu} + i\lambda^3 \epsilon \left(\frac{M^2}{\beta^2} - N \right) \left[\frac{f_1}{2+\nu} - \frac{f_2}{1+\nu} + \right. \\
 & \quad \left. \frac{f_{3+\nu}}{(1+\nu)(2+\nu)} \right] \tag{77}
 \end{aligned}$$

where $\nu = 0$ for the lift and $\nu = 1$ for the moment. The functions f_n , given by

$$f_n(M, \lambda) = \int_0^1 x^n e^{-i\lambda M^2 x / \beta^2} J_0 \left(\frac{M}{\beta^2} \lambda x \right) dx \tag{78}$$

arise in linearized theory for n ranging from 0 to 3. They have been studied and tabulated by von Borbely (ref. 17), Schwarz (ref. 18), and Garrick and Rubinow (ref. 11). They can all be expressed in terms of f_0 by a recurrence relation due to von Borbely (see, e.g., eq. (A.87) of ref. 12), so that the additional f_4 required here is easily computed.

Sketch (m) shows the variation of aerodynamic damping moment,



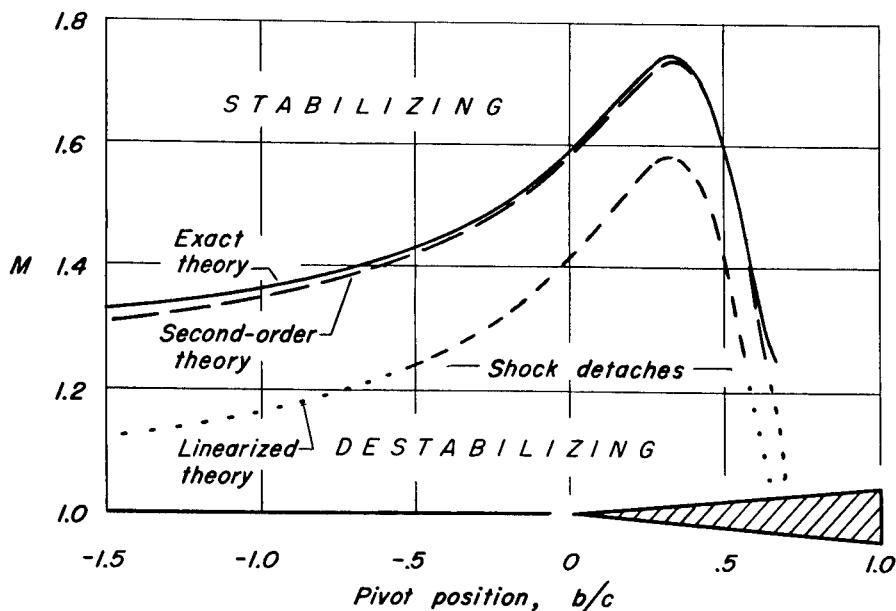
Sketch (m).- Damping moment coefficient for 10-percent-thick wedge oscillating about its vertex at $M = 10/7$.

according to first- and second-order theories, for a 10-percent-thick single wedge oscillating about its nose at a Mach number of $10/7$. Also shown for comparison are the parabolic approximations of the low-frequency analysis. It is seen that the thickness effect is reversed at high flutter frequencies, as is suggested by the parabolic approximation.

DISCUSSION

Higher-Order Effects

The moderate magnitude of second-order effects would suggest that the influence of third- and higher-order terms is of no practical importance, except perhaps in the transonic range near shock detachment. This supposition can be confirmed in the case of the single-wedge airfoil, for which a solution exact in thickness (but linearized with respect to angle of attack) has been derived in references 2 and 3. Sketch (n) compares the boundaries of neutral aerodynamic damping for a slowly oscillating wedge of 5° semivertex angle as predicted by the linearized,



Sketch (n).- Neutral damping boundary for wedge of 5° semivertex angle.

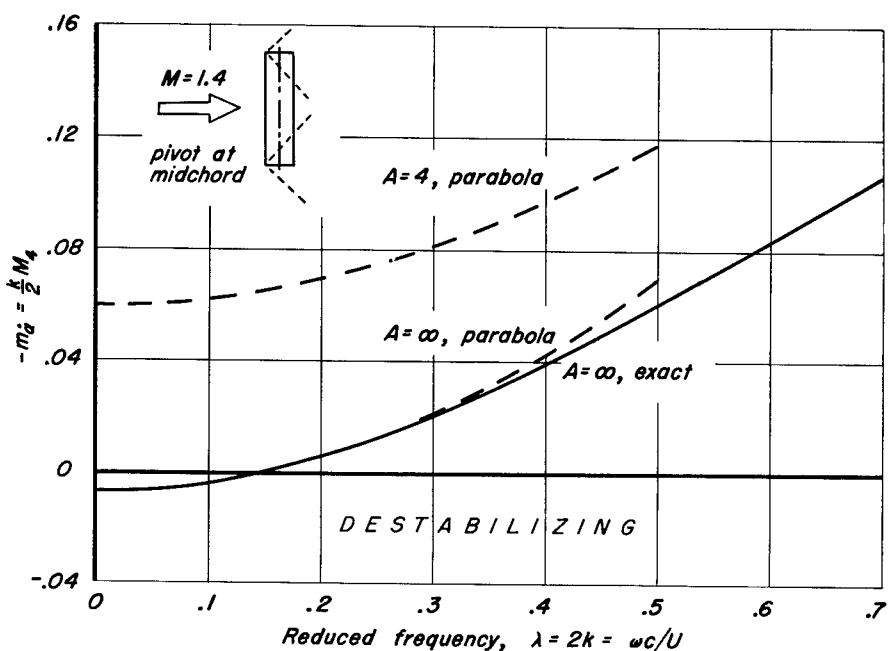
second-order, and exact theories. The second-order solution lies close to the exact result down to the Mach number for shock detachment (which is almost the same as the Mach number at which the flow ceases to be purely supersonic).

Application to Finite-Span Wings

Extension of the second-order solution to wings of finite aspect ratio does not seem possible at present. No second-order solution has yet been found even for steady flow past the simplest lifting wing.

Fortunately, the main conclusion to be drawn from the present analysis is that nonlinear thickness effects are quite moderate in magnitude. Practical supersonic wings will, therefore, probably be so thin that nonlinear effects are negligible, so that reliance can be placed in the predictions of linearized theory. Only if the wing is unduly thick, or if the Mach number is close to unity, or if unusual accuracy is required, may the engineer be forced to estimate the effects of thickness. In this event, he might assume that the effects of thickness are in some sense additive to those of aspect ratio, provided the aspect ratio is high and the frequency low. For example, the two-

dimensional correction might be applied stripwise to the spanwise loading predicted by linearized theory. Some indication of the extent to which such an assumption would be justified can be obtained by considering other pairs of effects whose combined influence is known. Sketches (l) and (m) show that the effects of thickness and frequency are roughly additive for the frequencies of usual practical interest in dynamic stability analysis (say $\lambda < 0.2$). Likewise, sketch (o) shows that the



Sketch (o).- Effect of aspect ratio upon damping moment coefficient for rectangular wing according to linearized theory.

effects of aspect ratio and frequency, determined from Watkins' linearized solution for the rectangular wing (ref. 19), are nearly additive in the same range of frequencies.

Recently, Martin and Gerber have calculated the second-order effects of thickness upon damping in roll for wings of infinite span (ref. 20). They then estimate the effect for a finite rectangular wing by increasing the result of linearized theory in the same ratio as for the infinite wing. Agreement with experiment is thus considerably improved, which gives further assurance that superposition of thickness effects may be justified also for oscillating wings.

Further Analysis

If thickness effects of the magnitude indicated by the present analysis are judged to be significant at flutter frequencies, extension of the high-frequency solution to more practical profiles would be warranted. The solution given for a single wedge at arbitrary frequency should be extended next to the biconvex or double-wedge airfoil. Although considerable computation is involved, it does not appear that the labor would be prohibitive.

Ames Aeronautical Laboratory
National Advisory Committee for Aeronautics
Moffett Field, Calif., April 20, 1953

APPENDIX

SYMBOLS

a	speed of sound
A	aspect ratio of wing
b	downstream distance from leading edge to pivot
c	airfoil chord
C(s)	constant of integration
c _l	section lift coefficient
c _m	section moment coefficient
c _p	pressure coefficient
c _{p0}	surface pressure coefficient in mean steady flow
c _{p_u} , c _{p_l}	pressure coefficients on upper and lower surfaces of airfoil, respectively
g(x)	function defining upper surface of airfoil at zero angle of attack
h(t)	elevation of plunging airfoil
h(x)	function defining amplitude of oscillation of upper surface of smooth airfoil
k	reduced frequency, $\frac{\omega c}{2U}$
m _α , M ₄	aerodynamic damping coefficients (See eq. (66))
M	free-stream Mach number
N	$\frac{\gamma+1}{2} \frac{M^2}{\beta^2}$
p	static pressure
→ q	velocity vector
s	Laplace transformation variable

$s(x,y,t)$	function defining moving surface
t	time
u,v	velocity components parallel and perpendicular to free stream
U	free-stream velocity
$w(x)$	downwash velocity at $y = 0$
x,y	coordinates parallel and perpendicular to free stream
$Y(x)$	ordinate of upper surface of airfoil at zero angle of attack
z	$x - \beta y$
α	angle of attack
α_0	angular amplitude of oscillation
β	$\sqrt{M^2 - 1}$
γ	adiabatic exponent of gas
Δ	Laplacian operator, $\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$
ϵ	small parameter representative of airfoil thickness
κ	$\frac{M^2 \omega}{\beta^2 U}$
λ	reduced frequency, $\frac{\omega c}{U}$
ν	constant which is 0 or 1 in equation (74)
ρ	density
τ	airfoil thickness ratio
Φ	first-order mean steady perturbation potential
ϕ	second-order mean steady perturbation potential
Φ	complete perturbation potential
Ψ	first-order time-dependent perturbation potential
Ψ	second-order time-dependent perturbation potential

Ψ_*	partial particular integral of time-dependent iteration equation
ω	angular frequency of oscillation
Ω	complete velocity potential
$()_0$	free-stream conditions
$()_1$	conditions in mean steady flow behind bow shock wave on wedge
(\cdot)	differentiation with respect to time
$(\bar{ })$	
$L\{ \}$	Laplace transform

REFERENCES

1. Busemann, A.: Aerodynamischer Auftrieb bei Überschallgeschwindigkeit. *Luftfahrtforschung*, Bd. 12, Nr. 6, Oct. 3, 1935, p. 213. (Reprinted in: *Foundations of High Speed Aerodynamics*, George F. Carrier, ed., Dover Publications, 1951, p. 134.)
2. Carrier, G. F.: The Oscillating Wedge in a Supersonic Stream. *Jour. Aero. Sci.*, vol. 16, no. 3, Mar. 1949, pp. 150-152.
3. Van Dyke, Milton D.: On Supersonic Flow Past an Oscillating Wedge. (To be published in the *Quart. Appl. Math.*)
4. Courant, R., and Friedrichs, K.O.: *Supersonic Flow and Shock Waves*. Interscience Publishers, Inc., 1948.
5. Van Dyke, Milton D.: A Study of Second-Order Supersonic Flow Theory. NACA Rep. 1081, 1952 (Supersedes NACA TN 2200).
6. Lamb, Horace: *Hydrodynamics*. Sixth ed., Dover Publications, 1945, p.7.
7. Magnus, Wilhelm, and Oberhettinger, Fritz (John Wermer, trans.): *Formulas and Theorems for the Special Functions of Mathematical Physics*. Chelsea Pub. Co. (New York City), 1949, pp. 120-136.
8. Karp, S. N., Shu, S. S., and Weil, H.: Aerodynamics of the Oscillating Airfoil in Compressible Flow. Monograph III. Air Materiel Command Tech. Rep. No. F-TR-1167-ND, Oct. 1947.
9. Van Dyke, Milton D.: On Second-Order Supersonic Flow Past a Slowly Oscillating Airfoil. *Jour. Aero. Sci.*, vol. 20, no. 1, Jan. 1953, p.61.
10. Lighthill, M. J.: Oscillating Airfoils at High Mach Number. (To be published in *Jour. Aero. Sci.*)
11. Garrick, I. E., and Rubinow, S. I.: Flutter and Oscillating Air-Force Calculations for an Airfoil in a Two-Dimensional Supersonic Flow. NACA Rep. 846, 1946. (Supersedes NACA TN 1158).
12. Temple, G., and Jahn, H. A.: Flutter at Supersonic Speeds: Derivative Coefficients for a Thin Aerofoil at Zero Incidence. R. & M. No. 2140, British A.R.C., 1949.

13. Jones, W. P.: The Influence of Thickness Chord Ratio on Supersonic Derivatives for Oscillating Aerofoils. To be published as R. & M. No. 2679, British A.R.C. (Supersedes A.R.C. Rep. No. 10,871, 1947).
14. Wyllie, Alexander: A Second-Order Solution for an Oscillating Two-Dimensional Supersonic Airfoil. Ph. D. Thesis, Caltech, 1951. Published in abridged form, Jour. Aero. Sci., vol. 19, no. 10, Oct. 1952, pp. 685-696, 704.
15. Beavan, J. A., and Holder, D. W.: Recent Developments in High-Speed Research - in the Aerodynamics Division of the National Physical Laboratory. Jour. Roy. Aero. Soc., vol. 54, no. 477, Sept. 1950, pp. 571-572.
16. Jones, W.P., and Skan, Sylvia W.: Aerodynamic Forces on Biconvex Aerofoils Oscillating in a Supersonic Airstream. To be published as R. & M. No. 2749, British A.R.C. (Supersedes A.R.C. Rep. No. 13,162, 1950.)
17. von Borbely, S.: Über die Luftkräfte die auf einen harmonisch schwingenden zweidimensionalen Flügel bei Überschallgeschwindigkeit wirken. ZWB FB 1071, Nov. 1939.
18. Schwarz, L.: Untersuchung einiger mit den Zylinderfunktionen nullter Ordnung verwandter Funktionen. Luftfahrtforschung, Bd. 20, Lfg. 12, 1944, pp. 341-372.
19. Watkins, Charles E.: Effect of Aspect Ratio on the Air Forces and Moments of Harmonically Oscillating Thin Rectangular Wings in Supersonic Potential Flow. NACA Rep. 1028, 1951 (Supersedes NACA TN 2064).
20. Martin, John C., and Gerber, Nathan: On the Effect of Thickness on the Damping in Roll of Airfoils at Supersonic Speeds. Ballistic Research Laboratories, Aberdeen Proving Ground, Md., Rep. No. 843, Jan. 1953.

NACA TN 2982

National Advisory Committee for Aeronautics.
SUPERSONIC FLOW PAST OSCILLATING AIRFOILS
INCLUDING NONLINEAR THICKNESS EFFECTS.
Milton D. Van Dyke. July 1953. 41p. diagrs.
(NACA TN 2982)

A solution to second order in thickness is derived for harmonically oscillating two-dimensional airfoils in supersonic flow. For slow oscillations of an arbitrary profile, the result is found as a series including the third power of frequency. For arbitrary frequencies, the method of solution for any specific profile is indicated, and the explicit solution derived for a single wedge. Nonlinear thickness effects are found generally to reduce the torsional damping, and so enlarge the range of Mach numbers within which torsional instability is possible.

Copies obtainable from NACA, Washington



1. Flow, Supersonic (1.1.2.3)
2. Wing Sections - Thickness (1.2.1.2.2)
3. Damping Derivatives - Stability (1.8.1.2.3)
4. Vibration and Flutter (4.2)

I. Van Dyke, Milton Denman
II. NACA TN 2982

A solution to second order in thickness is derived for harmonically oscillating two-dimensional airfoils in supersonic flow. For slow oscillations of an arbitrary profile, the result is found as a series including the third power of frequency. For arbitrary frequencies, the method of solution for any specific profile is indicated, and the explicit solution derived for a single wedge. Nonlinear thickness effects are found generally to reduce the torsional damping, and so enlarge the range of Mach numbers within which torsional instability is possible.



1. Flow, Supersonic (1.1.2.3)
2. Wing Sections - Thickness (1.2.1.2.2)
3. Damping Derivatives - Stability (1.8.1.2.3)
4. Vibration and Flutter (4.2)

NACA TN 2982
National Advisory Committee for Aeronautics.
SUPERSONIC FLOW PAST OSCILLATING AIRFOILS
INCLUDING NONLINEAR THICKNESS EFFECTS.
Milton D. Van Dyke. July 1953. 41p. diagrs.
(NACA TN 2982)



NACA TN 2982

National Advisory Committee for Aeronautics.
SUPERSONIC FLOW PAST OSCILLATING AIRFOILS
INCLUDING NONLINEAR THICKNESS EFFECTS.
Milton D. Van Dyke. July 1953. 41p. diagrs.
(NACA TN 2982)

A solution to second order in thickness is derived for harmonically oscillating two-dimensional airfoils in supersonic flow. For slow oscillations of an arbitrary profile, the result is found as a series including the third power of frequency. For arbitrary frequencies, the method of solution for any specific profile is indicated, and the explicit solution derived for a single wedge. Nonlinear thickness effects are found generally to reduce the torsional damping, and so enlarge the range of Mach numbers within which torsional instability is possible.



1. Flow, Supersonic (1.1.2.3)
2. Wing Sections - Thickness (1.2.1.2.2)
3. Damping Derivatives - Stability (1.8.1.2.3)
4. Vibration and Flutter (4.2)

I. Van Dyke, Milton Denman
II. NACA TN 2982

Copies obtainable from NACA, Washington



1. Flow, Supersonic (1.1.2.3)
2. Wing Sections - Thickness (1.2.1.2.2)
3. Damping Derivatives - Stability (1.8.1.2.3)
4. Vibration and Flutter (4.2)



Copies obtainable from NACA, Washington